

Curved waveguide having a ...

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$$\frac{1}{r} \frac{\partial}{\partial r} \left( r \frac{\partial W^{(n)}}{\partial r} \right) + \frac{1}{r^2} \frac{\partial^2 W^{(n)}}{\partial y^2} + \frac{\beta_n^2 W^{(n)}}{r^2} + k^2 W^{(n)} = 0. \quad (1)$$

Its solution is found in the form of a linear combination of the Bessel and Neumann functions:  $W_n = J_{\delta_n}(x) + \eta_n N_{\delta_n}(x) \quad (5).$

$\eta_n$  is a constant which has different values for different  $n$ .  $\delta_n$  is the solution of the transcendental equation:

$$J_{\delta_n}(y) N_{\delta_n}(\epsilon y) - J_{\delta_n}(\epsilon y) N_{\delta_n}(y) = 0 \quad (6).$$

$\delta_n^2 = -\beta_n^2$  and  $\beta$  denotes the propagation factor.  $\epsilon = R/q$ . It is pointed out that the numerical values  $W_n$ , i.e., the field distribution of the wave propagating in the guide cross section is very hard to calculate, since there is no table for Bessel functions of arbitrary fractions.

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The values of  $W_n$  ( $n > 1$ ) representing the distribution of the field for local waves cannot be calculated from (5), since  $\beta_n$  is not tabulated and the solution of (6) is very difficult for imaginary  $\delta_n$ . Therefore, explicit analytical formulas are derived here from elementary functions for  $W_n$  and  $\beta_n$ :

$$\begin{aligned} W_{n,m} + n^2 W_{n,m} = W_{n,0} [d_{n,m} + 2\alpha d_{n,m-1} + 3\alpha^2 d_{n,m-2} + \dots \\ \dots + m\alpha^{m-1} d_{n,1} + (m+1)\alpha^m d_{n,0}] + W_{n,1} [d_{n,m-1} + \\ + 2\alpha d_{n,m-2} + \dots + (m-1)\alpha^{m-2} d_{n,1} + m\alpha^{m-1} d_{n,0}] + \dots + \\ + W_{n,m-2} (d_{n,2} + 2\alpha d_{n,1} + 3\alpha^2 d_{n,0}) + W_{n,m-1} (d_{n,1} + 2\alpha d_{n,0}) + \\ + W_{n,m-1} + \alpha W_{n,m-2} + \dots + \alpha^{m-2} W_{n,1} + \alpha^{m-1} W_{n,0}. \quad (14) \end{aligned}$$

$$\beta_n = \Theta \left[ -\frac{0.25}{\Theta^2} + \left( z - 1 - \frac{1.5}{n^2 \Theta^2} \right) d_{n,0} + \left( \frac{z^2}{12n^2} - \frac{1.25}{n^4 \Theta^2} \right) d_{n,0}^2 \right]^{\frac{1}{2}}, \quad (18)$$

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where  $r = \frac{a}{\pi}(\theta - \alpha)$ ;  $\theta = \frac{\pi}{a}R$ ;  $q_n^2 = \beta_n^2/\theta^2$ ;  $m$  denotes the power of  $\theta$ .

$z = \pi/\theta = a/R$ . The curvature in the E-plane is investigated analogously. For this case, formula (5) is also valid, but  $x = \gamma r$  and  $\delta_n$  has to be found from the following equation:

$$\frac{J_{\delta_n}(y)}{n} N_{\delta_n}(y) - J_{\delta_n}(\epsilon y) N_{\delta_n}'(y) = 0 \quad (22),$$

where  $y = \gamma q$  and  $\epsilon = R/q$ . Again, the solution meets with the same difficulties mentioned above. The formulas for  $U_n$  and  $\beta_n$  are derived in analogous manner. For  $n \neq 0$  and  $n = 0$  various formulas are obtained. The zero-order approximation for  $n \neq 0$  has the form:

$$U_{n,0} = \cos na \quad (25)$$

$$\epsilon_{n,0} = q^2 - n^2 \quad (26),$$

where  $g_n^2 = \beta_n^2/\sigma^2$  and  $\sigma = \frac{\pi}{b}R$ ;  $q^2 = \gamma^2(b/\pi)^2 = (2b/\lambda_g)^2$ . The correction

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for the first approximation is given by:

$$U_{n,1} = \frac{g_{n,0}}{2n} \left( a^2 - \pi a - \frac{1}{n^2} - \frac{1}{g_{n,0}} \right) \sin n\alpha + \left( \frac{g_{n,0}}{2n^2} + \frac{1}{2} \right) a \cos n\alpha, \quad (27)$$

$$g_{n,1} = -\pi g_{n,0}.$$

and that for the second one reads:

$$\begin{aligned} U_{n,2} = & \left[ -\frac{g_{n,0}^2}{8n^3} a^4 + \frac{\pi g_{n,0}^2}{4n^3} a^2 + \left( \frac{3}{8} + \frac{10g_{n,0} - \pi^2 g_{n,0}^2}{8n^3} + \right. \right. \\ & \left. \left. + \frac{7g_{n,0}^2}{8n^4} \right) a^2 - \frac{3\pi g_{n,0}}{4n^3} \left( \frac{g_{n,0}}{n^2} + 1 \right) a \right] \csc n\alpha + \left[ \frac{g_{n,0}}{4n} \left( \frac{5g_{n,0}}{3n^3} + 3 \right) a^2 - \right. \\ & \left. - \frac{\pi g_{n,0}}{2n} \left( \frac{g_{n,0}}{n^3} + \frac{3}{2} \right) a^2 + \left( -\frac{3}{4n} + \frac{\pi^2 g_{n,0}^2 - 30g_{n,0}}{12n^3} - \frac{7g_{n,0}^2}{4n^3} \right) a + \right. \\ & \left. + \frac{3\pi g_{n,0}}{4n^3} \left( \frac{g_{n,0}}{n^3} + 1 \right) \right] \sin n\alpha, \end{aligned} \quad (28)$$

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$$g_{n,2} = -\frac{3}{4} - \frac{5g_{n,0}}{2n^3} - \left( \frac{\pi^2}{12n^2} + \frac{7}{4n^4} \right) g_{n,0}^2.$$

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43 For n = 0 these three formulas read as follows:

$$U_{0,0} = 1, \quad g_{0,0} = q^2, \quad (29) \quad (29)$$

$$U_{0,1} = \left( \frac{\pi}{3} - \frac{\pi}{2} \right) a^2 g_{0,0}, \quad g_{0,1} = -\pi g_{0,0}. \quad (30) \quad (30)$$

$$U_{0,2} = g_{0,0}^2 \frac{a^4}{45} - \frac{\pi}{15} g_{0,0}^2 a^2 + \left( \frac{g_{0,0}}{3} + \frac{\pi^2}{24} g_{0,0}^2 \right) a^4 - \\ - \frac{\pi}{2} g_{0,0} a^2 + \frac{\pi^2 g_{0,0}}{12} \left( 1 + \frac{\pi^2 g_{0,0}}{5} \right) a^2, \quad (31) \quad (31)$$

$$g_{0,2} = \frac{\pi^2}{6} g_{0,0} + \frac{\pi^4}{30} g_{0,0}^2, \quad g_{0,3} = 0. \quad (31).$$

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$$\beta_0 = i\beta = \sigma \left[ \left( z - 1 - \frac{z^2}{6} \right) g_{0,0} - \frac{\pi^2 z^2}{30} g_{0,0}^2 \right]^{\frac{1}{2}} \quad (32)$$

is the formula for the propagation factor of the fundamental wave, and

$$\beta_n = \sigma \left[ \frac{0.75}{n^2} + \left( z - 1 + \frac{2.5}{n^2 z^2} \right) g_{n,0} + \left( \frac{z^2}{12n^2} + \frac{7}{4n^4 z^2} \right) g_{n,0}^2 \right]^{\frac{1}{2}} \quad (33)$$

is the formula for the propagation factor (decrement of damping) of waves of higher order. Summing up: As far as the  $\beta$  values published by R. A. Waldron (Ref. 2: Journal of the British IRE, v. 17, no. 10, 1957) constitute a mathematically exact solution of Eqs. (6) and (22) and have also been confirmed experimentally by D. I. Voskresenskiy (Ref. 1: Trudy MAI, vyp. 73, 1957. (Interactions MAI, no. 73, 1957)), the values found for  $\beta$  from (18) and (32) have been compared with those obtained by interpolation from the tables of Ref. 2. A good agreement of the experimental values with those found by approximate and exact formulas proves the correctness of the approximate formulas for all  $\beta_n$ . Since the functions

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$W_n$  (and  $U_n$ ) and  $\beta_n$  are interconnected by (6) and (22), it can be assumed that the approximate formulas obtained for  $W_n$  and  $U_n$  will yield values closer to the actual values, and it can also be assumed that these formulas can be used to calculate the field of the fundamental wave and also that for waves of higher order. A similar method for solving the Bessel equation has also been applied by L. Lewin (Ref. 4: PIEE, part B, v. 102, no. 1, 1955). There are 4 figures and 5 references; 3 Soviet-bloc and 2 non-Soviet-bloc. The reference to the English-language publication reads as follows: R. A. Waldron. Journal of the British IRE, v. 17, no. 10, 1957.

ASSOCIATION: Nauchno-tehnicheskoye obshchestvo radiotekhniki i elektroniki im. A. S. Popova (Scientific and Technical Society of Radio Engineering and Electrical Communications imeni A. S. Popov) [Abstracter's note: Name of association was taken from first page of journal]

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KISLYUK, M.Zh.

Curved wave guide with a rectangular cross section. Radiotekhnika  
16 no.4:3-10 Ap '61. (MIRA 14:9)  
(Wave guides)

KISLYUK, M. Zh.,

"Investigation of Bent Waveguides of Rectangular Cross Section." Dissertation  
for the Degree of Candidate of Sciences, Leningrad Electrotechnic Inst. of Communication  
im. M. A. Bonch-Bruyevich. Defense held on 23 June 1960.

The structure of the electromagnetic field in a bent waveguide is investigated.  
A mathematical expression is obtained for the determination of the field structure. A  
procedure is proposed for the calculation of the coefficient of reflection in coupled  
straight and bent waveguides, which makes it possible to choose a rational radius of  
the bend. The set of theoretical and experimental work performed makes it possible  
to obtain scientifically justified and practically convenient calculations for the  
standing-wave coefficients of the waveguide bend.

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REEL #228

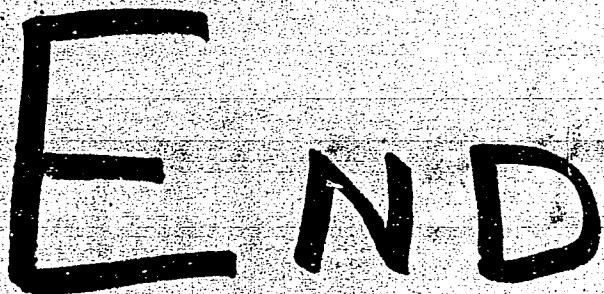
Kiselev, A. Ya.

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Kislyuk, M. Zh.

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